

The Crystal and Molecular Structure of Anthracene.

I. X-ray Measurements

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A very complete redetermination of the crystal structure of anthracene is described. All the reflexions that lie within the range of Cu $K\alpha$ radiation have been recorded on equi-inclination Weissenberg exposures, and the intensities have been estimated visually by independent observers. From these results a total of 691 structure factors have been evaluated out of a possible 1085 (64%). The earlier two-dimensional determination of the structure has been further refined, by revising the ($h0l$) structure factors and the (010) projection, and from these results it has now been possible to assign phase constants to 667 of the structure factors. These are used in a new three-dimensional determination of the structure which is described in Part II.

1. Introduction

A very complete redetermination of the crystal and molecular structure of naphthalene has recently been described (Abrahams, Robertson & White, 1949*a, b*). The present papers deal with a similar redetermination of the structure of anthracene, carried out by the same methods, and we hope with about the same degree of precision.

A survey of the earlier work on the crystal structure of anthracene is given in the papers referred to above. The 1933 determination by double Fourier series methods, employing the axial zones of reflexion (Robertson, 1933), was used as the starting point for the present investigation, which now embraces all the X-ray reflexions within the range of Cu $K\alpha$ radiation at room temperature. A total of 691 structure factors has been evaluated out of a possible 1085 which are theoretically within the range of this wave-length. The previous two-dimensional structure determination, after some further refinement, has enabled us to make a reliable assessment of the phase constants for 667 of these structure factors, and their utilization in a three-dimensional determination of the structure is described in Part II.

The number of reflexions observed in the case of anthracene amounts to 63.7% of those theoretically possible. For naphthalene the corresponding figure was 77.4%. The smaller figure for anthracene is difficult to explain. It may be due in part to somewhat less intense exposures, although an attempt was made to keep these the same as for naphthalene, and the intensity range covered in the ($h0l$) zone is comparable for the two crystals (about 5000 to 1). Part of the difference will be due to the anthracene structure being more complex, with a larger number of small structure factors. For anthracene $F(000)$ is 188, while for naphthalene it is 136. The number of recorded structure factors might be increased by the use of larger crystals and longer exposures, but the present list appears to contain most

of those whose sign (phase constant) can be determined with some measure of certainty from the 1933 approximation.

2. Crystal data

The crystal constants were redetermined by means of suitably calibrated oscillation and moving-film photographs. The following new values differ only slightly from the earlier measurements (Robertson, 1933):

Anthracene, $C_{14}H_{10}$; M , 178.2; m.p. $218^\circ C.$; d , calc. 1.24, found 1.25. Monoclinic prismatic,

$$a = 8.561 \pm 0.010, \quad b = 6.036 \pm 0.010, \\ c = 11.163 \pm 0.010 \text{ \AA.}, \quad \beta = 124^\circ 42' \pm 4'.$$

(The wave-length for Cu $K\alpha$ radiation was taken as 1.542 \AA.)

Absent spectra, ($h0l$) when h is odd; ($0k0$) when k is odd. Space group, $C_{2h}^5-P2_1/a$. Two molecules per unit cell. Molecular symmetry, centre. Volume of the unit cell, 474.2 \AA.³. Absorption coefficient for X-rays, $\lambda = 1.542 \text{ \AA.}$, $\mu = 6.45 \text{ cm.}^{-1}$. Total number of electrons per unit cell = $F(000) = 188$.

3. Experimental measurements

The X-ray work was carried out in a similar manner to that described for naphthalene (Abrahams *et al* 1949*a*) except that no special precautions were required to preserve the anthracene crystals. Suitable specimens were grown by slow cooling from amyl acetate solution. These were generally needle-shaped, elongated in the direction of the b axis.

The photographic surveys used for the intensity estimates were made exclusively on an instrument of the equi-inclination Weissenberg type. It was found that all the reflexions could be recorded, with sufficient overlap for correlation, on exposures of the equatorial and the first three, four or five layer lines for rotations about the [100], [010], [001] and [101] axes. Details

The discrepancies finally obtained between the measured and calculated F values in Table 3, expressed as

$$\frac{\Sigma(|F_{\text{meas.}}| - |F_{\text{calc.}}|)}{\Sigma|F_{\text{meas.}}|},$$

amount to 19.6% for all the values listed. This figure is reduced to 18.2% if $\Sigma|F_{\text{calc.}}|$ is used as denominator, because the scales of the measured and calculated values are not exactly correlated, the measured scale being based on certain absolute measurements made in the 1933 investigation. Nevertheless, the discrepancies are

clearly a little greater than in the naphthalene investigation. They could undoubtedly be improved if allowance were made for the hydrogen atoms and for the electron distribution between the carbon atoms in the rings.

References

- ABRAHAMS, S. C., ROBERTSON, J. M. & WHITE, J. G. (1949a). *Acta Cryst.* **2**, 233.
 ABRAHAMS, S. C., ROBERTSON, J. M. & WHITE, J. G. (1949b). *Acta Cryst.* **2**, 238.
 ROBERTSON, J. M. (1933). *Proc. Roy. Soc. A.* **140**, 79.
 TUNELL, G. (1939). *Amer. Min.* **24**, 448.

Table 3. Measured and calculated values of the anthracene structure factors

* Values omitted from the Fourier synthesis.

** Values included in the Fourier synthesis with incorrect sign.

hkl	$F_{\text{meas.}}$	$F_{\text{calc.}}$	hkl	$F_{\text{meas.}}$	$F_{\text{calc.}}$	hkl	$F_{\text{meas.}}$	$F_{\text{calc.}}$	hkl	$F_{\text{meas.}}$	$F_{\text{calc.}}$
001	32.8	+38.4	40 $\bar{0}$	26.6	+28.3	018	9.0	- 8.5	2.1.1 $\bar{2}$	<1.2	+ 1.0
002	23.7	-25.2	4.0.10	10.3	+10.3	019	9.8	- 9.2	2.1.1 $\bar{3}$	1.7	- 1.8
003	16.4	+15.0	4.0.11	3.7	- 3.7	0.1.10	<2.0	- 0.3	319	<0.9	- 2.1
004	24.6	-19.9	4.0.12	2.0	+ 2.0	0.1.11	<1.3	- 0.3	318	<1.6	- 2.5
005	16.9	-14.7	4.0.13	3.6	- 3.1	110	53.5	+65.0	317	2.0*	- 0.4
006	6.0	+ 6.0	605	<1.2	- 1.2	210	52.0	-47.8	316	2.1	- 0.3
007	<1.8	- 0.7	604	4.5	+ 3.5	310	11.7	+10.8	315	2.2	+ 1.4
008	4.1	- 4.4	603	<2.0	+ 0.1	410	28.3	-24.9	314	6.4	- 5.8
009	5.8	- 5.0	602	<2.1	- 0.7	510	5.0	- 5.6	313	4.8	- 3.9
0.0.10	<1.8	- 0.7	601	<2.1	+ 2.7	610	6.2	- 3.7	312	4.0	+ 5.4
0.0.11	1.5	+ 1.7	60 $\bar{1}$	11.2	-12.8	710	3.0	- 2.5	311	8.1	-10.0
020	22.7	-22.5	60 $\bar{2}$	2.9	- 3.1	810	<1.7	+ 0.6	31 $\bar{1}$	31.5	+28.9
040	3.7	- 1.6	60 $\bar{3}$	4.9	+ 5.1	910	<0.8	- 0.4	31 $\bar{2}$	3.9	- 3.8
060	<1.8	+ 1.8	604	4.6*	- 2.4	1.1.11	<0.9	+ 0.3	31 $\bar{3}$	2.6	+ 2.7
200	65.0	+73.8	60 $\bar{5}$	20.6	-18.4	1.1.10	<1.5	0.0	314	14.3	- 9.3
400	3.9	- 1.8	60 $\bar{6}$	5.3	- 4.0	119	2.4	- 2.4	31 $\bar{5}$	25.8	-20.7
600	7.3	- 8.3	607	2.0	+ 2.3	118	<2.1	+ 0.4	31 $\bar{6}$	<1.6	+ 2.7
800	2.5	- 1.5	60 $\bar{8}$	2.4	- 4.0	117	<1.7	- 0.1	317	0.9	- 2.7
2.0.10	<1.0	+ 0.9	609	16.4	+19.0	116	<1.7	+ 0.8	318	3.8	+ 3.9
209	4.3	- 5.7	6.0.10	16.6	+17.6	115	6.4	- 5.7	319	13.7	+13.0
208	5.5	- 7.5	6.0.11	3.8	- 3.9	114	19.3	-17.1	3.1.10	<1.4	- 0.4
207	<2.2	- 0.3	6.0.12	<2.0	0.0	113	6.0	+ 7.1	3.1.11	1.9	- 1.2
206	3.5	+ 4.0	6.0.13	<1.7	+ 1.9	112	<1.0	- 1.1	3.1.12	1.8	+ 1.8
205	9.3	- 8.3	6.0.14	3.0	- 3.2	111	12.4	- 7.9	3.1.13	3.5	- 2.7
204	25.5	-24.8	802	<1.0	- 1.1	11 $\bar{1}$	26.9	+29.4	417	<1.5	+ 2.3
203	4.4	- 2.5	801	<1.5	+ 0.5	11 $\bar{2}$	13.2	-14.5	416	1.9	- 2.6
202	4.3	+ 3.1	80 $\bar{1}$	7.4	- 8.7	11 $\bar{3}$	15.5	+12.6	415	3.3	+ 1.5
201	4.5	- 4.1	802	4.5	- 3.1	114	21.1	-17.0	414	10.5	+10.7
20 $\bar{1}$	43.5	+52.8	80 $\bar{3}$	2.1	+ 2.6	11 $\bar{5}$	19.5	-16.7	413	5.0	+ 3.1
20 $\bar{2}$	25.5	-28.8	804	<2.1	- 1.1	11 $\bar{6}$	<1.4	+ 1.5	412	<2.0	- 1.0
203	14.5	+12.5	805	10.3	- 9.6	117	<1.6	- 1.0	411	2.4	+ 2.7
204	3.3*	+ 2.4	80 $\bar{6}$	9.0	- 8.1	118	6.7	+ 5.3	41 $\bar{1}$	33.1	-36.1
205	5.0	-10.5	807	2.2	+ 2.6	119	3.6	+ 2.3	41 $\bar{2}$	2.7	+ 3.3
206	5.4	+ 7.4	808	<2.1	- 0.7	1.1.10	2.8	- 2.8	413	5.2	+ 7.3
207	4.4	- 5.3	809	2.1	+ 1.9	1.1.11	<1.4	+ 1.1	414	16.4	-16.8
208	2.6	+ 3.0	8.0.10	9.0	+ 9.0	1.1.12	<1.0	- 0.8	41 $\bar{5}$	10.2	- 7.6
209	9.2	+10.4	8.0.11	<1.9	- 0.4	2.1.10	<0.9	- 0.1	416	2.0	+ 2.0
2.0.10	<1.6	+ 0.1	8.0.12	1.4	- 1.4	219	<1.6	- 1.1	417	1.8	- 2.8
2.0.11	<1.5	+ 0.8	8.0.13	1.5	+ 2.8	218	<2.0	- 0.7	418	3.1	+ 4.2
2.0.12	<1.2	- 0.2	8.0.14	<1.0	- 1.3	217	<2.2	+ 1.7	419	9.4	+10.4
2.0.13	<0.7	- 5.2	10.0.3	<1.1	+ 0.9	216	<2.2	- 1.7	4.1.10	3.1	+ 2.6
408	3.2	- 4.2	10.0.4	<1.4	- 1.2	215	<1.5	- 1.9	4.1.11	2.2	- 2.3
407	<1.5	0.0	10.0.5	<1.5	- 0.9	214	1.9	+ 0.9	4.1.12	<1.9	+ 0.8
406	<1.8	+ 0.8	10.0.6	<1.7	- 3.3	213	4.0	- 4.0	4.1.13	<1.5	- 1.6
405	<2.1	- 1.8	10.0.7	<1.7	- 0.5	212	3.8	+ 5.3	516	<1.4	- 0.9
404	8.4	- 7.9	10.0.8	<1.7	+ 1.7	211	1.7	+ 0.4	515	1.8	+ 1.5
403	7.6	- 8.0	10.0.9	1.9	- 2.7	21 $\bar{1}$	40.5	-42.3	514	2.9	+ 3.0
402	3.7	+ 5.1	10.0.10	1.8	- 2.3	21 $\bar{2}$	9.1	+ 8.5	513	3.1	- 3.2
401	<1.7	- 1.1	10.0.11	<1.4	- 0.5	213	1.2	+ 3.0	512	<1.7	+ 0.5
40 $\bar{1}$	3.5	+ 7.5	10.0.12	<1.1	0.0	214	6.9	- 6.8	511	<2.1	+ 0.2
40 $\bar{2}$	6.3	- 7.2	011	10.7	+10.4	215	13.2	+11.5	51 $\bar{1}$	6.0	+ 5.4
40 $\bar{3}$	6.2	+ 5.1	012	3.6	+ 3.4	216	2.4	+ 3.5	51 $\bar{2}$	4.1	+ 2.9
404	1.8	+ 1.1	013	3.9	- 3.2	217	6.5	- 7.3	51 $\bar{3}$	1.6*	- 0.8
405	12.3	-13.9	014	11.9	- 9.6	218	11.1	+11.0	514	3.8	- 3.2
406	5.0	+ 6.0	015	16.0	-13.6	219	16.5	+17.5	515	16.2	-15.2
407	5.2	- 5.0	016	<2.1	- 0.4	2.1.10	2.9	+ 2.7	51 $\bar{6}$	<1.3	- 0.3
408	1.6**	+ 0.6	017	3.6	- 4.4	2.1.11	2.0	- 1.8	517	2.0	+ 2.2

Table 3 (cont.)

<i>hkl</i>	<i>F</i> _{meas.}	<i>F</i> _{calc.}	<i>hkl</i>	<i>F</i> _{meas.}	<i>F</i> _{calc.}	<i>hkl</i>	<i>F</i> _{meas.}	<i>F</i> _{calc.}	<i>hkl</i>	<i>F</i> _{meas.}	<i>F</i> _{calc.}
51 $\bar{8}$	2.8	- 3.5	10.1 $\bar{7}$	<1.1	- 0.6	322	1.2	- 1.7	722	5.8	- 4.5
519	12.5	+13.3	10.1 $\bar{8}$	<1.6	+ 0.2	321	2.1	+ 3.1	723	<1.3	0.0
5.1.10	7.4	+ 7.7	10.1 $\bar{9}$	2.0	- 1.5	32 $\bar{1}$	24.7	-25.0	724	3.9	+ 2.7
5.1.11	3.0	- 3.0	10.1.10	7.6	- 7.3	32 $\bar{2}$	4.7	+ 6.8	725	8.2	+ 6.9
5.1.12	2.9	+ 2.1	10.1.11	1.7	- 2.4	32 $\bar{3}$	3.8**	+ 2.4	726	2.5	+ 1.8
5.1.13	<1.6	- 1.0	10.1.12	<1.0	+ 2.1	324	10.6	-13.4	727	<1.3	- 0.9
5.1.14	3.2	- 3.5	11.1.8	<0.5	+ 1.0	325	6.3	+ 5.9	728	<1.3	+ 0.3
615	<1.1	+ 0.3	11.1.9	<0.8	- 1.0	326	9.7	+ 9.1	729	5.4	- 5.9
614	8.2	+ 8.5	021	17.8	-18.9	327	3.2	- 3.7	7.2.10	4.8	- 5.1
613	7.4	+ 6.3	022	8.7	+ 5.6	328	1.3	+ 0.8	7.2.11	1.2	+ 1.2
612	<1.6	- 1.6	023	4.9*	0.0	329	8.8	+10.6	7.2.12	<1.2	- 0.1
611	<2.2	+ 0.4	024	17.9	-15.7	3.2.10	3.0	+ 3.9	7.2.13	3.0	- 2.6
61 $\bar{1}$	12.6	-10.9	025	1.1	+ 1.8	3.2.11	<1.2	- 1.0	821	<0.8	+ 1.5
61 $\bar{2}$	<1.1	- 0.1	026	<1.2	- 1.5	3.2.12	<0.9	+ 1.5	82 $\bar{1}$	2.3	+ 1.9
61 $\bar{3}$	2.0	+ 3.2	027	<1.4	- 1.1	3.2.13	<0.6	- 1.3	82 $\bar{2}$	3.8	+ 4.6
614	6.0	- 7.2	028	12.4	+10.9	427	<0.8	+ 0.9	82 $\bar{3}$	<1.3	- 3.4
615	5.9	- 6.3	029	4.1	+ 3.3	426	<1.0	- 2.3	824	3.7	+ 3.4
61 $\bar{6}$	1.8	- 1.5	0.2.10	2.0	- 2.2	425	6.7	+ 6.6	825	8.4	+ 9.3
617	1.5	+ 1.0	0.2.11	<0.9	+ 0.8	424	8.6	+ 8.3	826	<1.4	- 0.4
618	<2.0	+ 1.4	120	20.5	-22.1	423	<1.3	- 1.6	827	<1.3	+ 0.4
619	4.5	- 4.2	220	13.1	-12.3	422	1.1	+ 2.0	828	<1.3	- 0.6
6.1.10	6.1	- 5.4	320	28.1	-26.4	421	4.7	- 4.5	829	2.7	- 4.1
6.1.11	<0.8	- 0.9	420	2.2	- 2.5	42 $\bar{1}$	20.8	+19.7	8.2.10	2.5	+ 2.3
6.1.12	<2.0	+ 0.8	520	9.0	- 7.1	42 $\bar{2}$	5.8	+ 5.7	8.2.11	2.3	+ 2.1
6.1.13	<1.7	+ 0.5	620	<1.3	- 1.0	42 $\bar{3}$	4.2	- 4.4	8.2.12	<0.9	- 0.4
6.1.14	1.5	+ 1.8	720	<1.3	- 0.3	424	4.5	- 4.3	8.2.13	2.2	- 1.5
713	2.0	+ 1.6	820	<0.9	- 1.0	425	19.3	-18.4	921	<0.7	- 1.3
712	2.1	- 2.1	1.2.10	<1.0	+ 1.2	426	5.9	- 5.2	922	<0.9	- 0.3
711	<2.0	+ 1.9	129	3.2	- 3.6	427	2.4	+ 3.7	923	<1.0	- 0.7
71 $\bar{1}$	5.4	- 4.2	128	8.0	- 7.4	428	2.3	- 2.5	924	2.3*	+ 0.9
71 $\bar{2}$	<1.7	+ 0.4	127	2.4	- 1.6	429	2.7	- 3.6	925	2.9	+ 7.5
71 $\bar{3}$	<1.2	- 0.3	126	1.7	+ 0.8	4.2.10	6.5	- 5.4	926	4.8	+ 3.8
714	<1.5	+ 0.3	125	5.0	+ 5.0	4.2.11	<1.3	- 0.6	927	<1.2	- 2.4
715	6.9	- 5.8	124	9.0	+ 6.9	4.2.12	<1.2	+ 1.4	928	<1.2	+ 1.7
716	3.7	- 4.1	123	0.9*	0.0	4.2.13	2.2	- 1.6	929	2.5	- 1.8
717	2.7	+ 3.6	122	<0.5	+ 0.7	526	<0.7	- 1.0	9.2.10	7.0	- 7.8
718	3.1	- 3.6	121	10.6	-10.8	525	2.9	+ 1.8	9.2.11	2.1	- 2.2
719	4.3	+ 2.9	12 $\bar{1}$	5.2*	+ 1.3	524	9.6	+ 9.4	9.2.12	<0.8	+ 1.1
7.1.10	9.2	+ 9.4	122	6.1	+ 8.6	523	4.5	+ 3.0	9.2.13	<0.5	- 1.8
7.1.11	<1.2	- 0.2	123	9.4	- 9.8	522	1.9	- 3.3	10.2.4	<0.7	+ 0.7
7.1.12	<0.8	- 0.2	124	13.5	- 9.4	521	2.6	+ 4.1	10.2.5	6.5	+ 5.7
7.1.13	<1.6	+ 0.6	125	3.0	+ 5.0	52 $\bar{1}$	26.7	-21.2	10.2.6	<0.9	+ 1.0
7.1.14	5.2	- 3.4	126	1.5	+ 2.9	52 $\bar{2}$	6.1	- 4.4	10.2.7	<0.9	- 1.4
812	<0.7	- 0.1	127	1.8	- 2.6	52 $\bar{3}$	1.0	+ 2.4	10.2.8	<0.9	+ 0.9
811	<1.5	- 0.6	128	11.3	+ 8.9	524	1.0	- 3.0	10.2.9	<0.9	- 1.3
81 $\bar{1}$	<2.0	+ 0.8	129	13.0	+10.9	525	5.6	+ 3.3	10.2.10	3.8	+ 3.3
81 $\bar{2}$	2.1	+ 2.1	1.2.10	<1.2	- 0.5	526	6.6	+ 5.7	10.2.11	4.6	+ 4.2
813	<2.0	- 0.1	1.2.11	<0.9	- 0.3	527	<1.2	0.0	031	20.9	-18.7
814	<2.2	- 1.8	1.2.12	<0.6	+ 1.6	528	2.2	- 3.8	032	<1.3	- 0.4
815	5.5	+ 3.7	229	<0.8	+ 0.2	529	1.3**	- 0.5	033	8.0	+ 6.9
816	3.5	+ 2.0	228	6.7	+ 7.4	5.2.10	1.8	+ 2.8	034	14.4	+12.9
817	<2.1	- 0.5	227	<1.3	+ 1.1	5.2.11	<1.3	+ 1.0	035	16.6	+15.5
818	<1.2	+ 1.8	226	2.1	- 3.4	5.2.12	<1.2	- 0.5	036	5.4	+ 2.9
819	7.1	- 6.1	225	11.2	+10.8	5.2.13	<0.9	- 1.0	037	2.2	- 2.2
8.1.10	12.5	-11.6	224	5.4	+ 4.2	625	<0.5	+ 1.8	038	3.5	- 2.7
8.1.11	2.3	- 1.8	223	2.8	- 1.9	624	3.6	+ 3.9	039	2.0	- 2.0
8.1.12	2.1	+ 2.3	222	6.2	+ 5.8	623	<1.0	- 1.8	0.3.10	<1.2	+ 0.8
8.1.13	1.7	- 1.8	221	13.3	-16.1	622	<1.3	- 0.7	130	21.5	-21.4
8.1.14	<0.7	- 0.9	22 $\bar{1}$	4.4	+ 5.2	621	<1.3	+ 0.9	230	3.7*	- 2.5
911	4.3	- 3.6	222	0.7	+ 2.0	62 $\bar{1}$	13.4	+12.3	330	7.5	- 6.5
912	1.7	- 1.4	223	<0.7	+ 1.1	62 $\bar{2}$	9.1	+ 7.9	430	1.8	- 1.7
913	<1.7	- 0.2	224	23.8	-23.0	623	4.7	- 6.3	530	1.2	- 3.1
914	<2.0	+ 0.4	225	20.1	-20.6	624	5.3	+ 5.6	630	<1.8	- 1.2
915	<2.1	+ 1.0	226	<0.6	- 1.0	625	1.6	+ 2.0	730	2.8	- 4.2
916	2.4	- 2.7	227	<0.7	- 0.3	626	3.4	- 4.5	830	1.9	- 1.2
917	<2.0	+ 0.2	228	5.5	+ 5.8	627	<1.3	+ 3.4	1.3.10	1.3	- 2.1
918	<1.9	+ 0.2	229	3.5	+ 2.5	628	2.8	- 3.3	139	<1.0	- 0.1
919	<1.1	- 2.4	2.2.10	4.7	- 4.6	629	4.8	- 6.4	138	8.0	+ 8.1
9.1.10	3.5	+ 3.6	2.2.11	<1.2	+ 0.4	6.2.10	1.8	- 2.1	137	<1.8	- 0.9
9.1.11	2.0	+ 2.2	2.2.12	<0.8	+ 0.6	6.2.11	<1.3	- 0.2	136	2.9*	+ 0.8
9.1.12	<1.0	- 0.9	328	<1.0	- 2.2	6.2.12	<1.2	+ 1.2	135	16.0	+16.7
9.1.13	<0.7	+ 0.2	327	1.2	- 1.1	6.2.13	4.1	- 3.0	134	3.5*	- 2.3
10.1.3	<0.9	- 0.6	326	<1.3	- 1.0	723	4.6	+ 4.0	133	13.4	-12.2
10.1.4	<1.4	- 1.4	325	8.4	+ 6.5	722	<0.9	- 0.6	132	3.7	+ 4.6
10.1.5	5.1	+ 5.8	324	11.6	+11.6	721	<1.2	+ 0.9	131	8.4	- 7.1
10.1.6	8.4	+ 5.8	323	<1.2	- 2.2	72 $\bar{1}$	8.3	- 7.1	13 $\bar{1}$	12.9	-14.9

Table 3 (cont.)

<i>hkl</i>	$F_{\text{meas.}}$	$F_{\text{calc.}}$	<i>hkl</i>	$F_{\text{meas.}}$	$F_{\text{calc.}}$	<i>hkl</i>	$F_{\text{meas.}}$	$F_{\text{calc.}}$	<i>hkl</i>	$F_{\text{meas.}}$	$F_{\text{calc.}}$
132	<1.3	-0.1	531	8.7	+8.7	044	1.9*	-0.5	442	7.9	-8.6
133	3.4	-3.6	532	<1.6	+0.6	045	13.2	+12.5	443	5.9	+5.3
134	10.1	-10.3	533	<1.5	-2.3	046	6.8	+5.8	444	15.4	+15.2
135	8.9	+8.8	534	13.1	+14.6	047	3.4	-4.6	445	5.5	+4.9
136	8.1	+7.0	535	<1.5	+0.9	048	1.5	-1.4	446	5.0	+3.3
137	4.3	-4.6	536	8.1	-8.9	049	2.3	-1.9	447	2.8	+1.5
138	2.6	+2.5	537	<1.2	+1.3	0.4.10	2.6	-2.1	448	3.8	-3.5
139	<1.7	+1.2	538	2.0	-1.9	140	<1.5	+1.7	449	1.2	-1.0
1.3.10	1.6	-2.1	539	6.9	-7.3	240	1.9	-1.8	4.4.10	<0.9	0.0
1.3.11	<1.1	+1.3	5.3.10	4.8	-4.9	340	1.5*	-0.1	4.4.11	<1.9	0.0
239	2.8	-1.8	5.3.11	<1.6	0.0	440	2.9	-3.5	4.4.12	<1.0	-1.0
238	5.6	-5.9	5.3.12	<1.4	-0.8	540	3.0	-3.3	544	<2.5	-2.3
237	4.6	-3.6	5.3.13	<0.9	-3.2	640	<3.0	-4.8	543	3.2	+2.5
236	2.4	+1.6	634	<1.0	-0.3	740	<2.3	-1.9	542	<1.5	+2.3
235	11.4	+10.5	633	<1.4	+0.5	148	<1.3	+0.8	541	<2.5	-1.0
234	13.6	+12.3	632	<1.4	-0.8	147	5.0	+1.0	541	3.4	+7.4
233	5.5	+2.7	631	<1.8	+2.0	146	<1.8	+1.4	542	4.3	+3.3
232	1.0*	+1.0	631	8.2	-6.8	145	8.7	+7.7	543	3.5*	+0.6
231	6.8	-4.9	632	6.8	-5.2	144	5.9	+4.3	544	9.8	+11.0
231	12.4	+15.5	633	<1.7	-0.1	143	1.1	+0.6	545	6.4	+5.9
232	2.2	+4.4	634	10.8	+9.1	142	2.5	+4.2	546	4.4	-4.4
233	3.5	-6.2	635	14.3	+12.2	141	3.8	-4.8	547	<2.1	+1.7
234	1.1	-2.1	636	6.3	+4.3	141	8.6	+9.9	548	<1.4	-0.4
235	4.6	-5.4	637	<1.3	+1.2	142	1.5	-3.7	549	1.9	-3.0
236	2.1	-0.4	638	2.2	-2.5	143	5.7	+6.1	5.4.10	2.4	+2.3
237	<1.5	+0.5	639	2.7	-3.0	144	5.0	+6.1	5.4.11	<1.2	0.0
238	3.2	-4.1	6.3.10	4.0	+4.1	145	13.0	-13.8	5.4.12	<1.4	-0.5
239	<1.6	-0.3	6.3.11	2.8	+2.8	146	9.3	-6.5	643	<1.0	-1.5
2.3.10	<1.4	+0.8	6.3.12	2.0	-1.9	147	<1.8	+0.2	642	<1.2	+0.5
2.3.11	<1.2	-0.2	6.3.13	<1.0	-1.5	148	4.7	-5.3	641	<2.2	-0.9
2.3.12	<0.8	+0.4	732	<1.1	+1.1	149	<1.5	-1.0	641	<0.9	-0.5
338	4.0	+5.0	731	<1.4	+0.4	1.4.10	3.5	+2.9	642	1.6	-1.3
337	4.1	+3.8	731	6.5	+5.8	248	<1.2	+1.9	643	<1.5	-1.3
336	<1.2	-2.3	732	8.2	+7.5	247	<1.2	+0.3	644	8.3	+8.5
335	8.0	+7.9	733	<1.8	-3.4	246	<1.4	-0.6	645	3.2	+2.8
334	5.5	+5.3	734	8.9	+7.5	245	5.1	+5.3	646	2.9	-4.4
333	6.2	-6.8	735	8.1	+8.6	244	<1.6	-2.0	647	<1.4	+0.7
332	1.3	+2.7	736	5.3	-6.2	243	6.7	-7.2	648	<2.0	+0.7
331	0.9*	-0.3	737	1.1	-1.0	242	<1.1	+1.0	649	<1.3	-0.8
331	4.3	-2.4	738	<1.5	+0.2	241	1.4	+0.7	6.4.10	1.4	-1.4
332	5.6	-6.5	739	3.7	-4.5	241	8.2	-8.1	6.4.11	1.8	-1.8
333	2.5	+3.1	7.3.10	3.3	-3.9	242	4.7	-6.5	6.4.12	<1.1	+0.9
334	3.3	+3.7	7.3.11	1.5	-1.5	243	8.5	+9.1	741	<1.4	-1.4
335	3.2	-4.9	7.3.12	<1.2	+0.1	244	9.4	+8.8	741	3.0	-1.9
336	2.1	+1.1	7.3.13	<1.4	-1.2	245	10.2	+10.0	742	<0.8	-0.3
337	<1.3	-0.9	831	7.6	-5.8	246	10.5	+10.7	743	<1.1	+0.1
338	4.5	-4.2	832	7.9	-5.5	247	2.2	-3.0	744	2.7	+1.6
339	3.7	-3.9	833	<1.7	-0.5	248	5.9	-5.3	745	5.0	+4.1
3.3.10	2.3	-2.5	834	5.9	+4.0	249	<1.4	-0.9	746	2.8	+2.1
3.3.11	1.1	+1.1	835	8.4	+6.8	2.4.10	<1.2	-0.7	747	1.5	+2.0
3.3.12	1.8	-1.8	836	3.9	+2.6	2.4.11	<0.8	+0.2	748	<1.3	+0.1
437	2.4	-2.8	837	<1.4	-0.4	347	<0.7	-1.3	749	<1.8	-1.4
436	<1.3	+0.4	838	<1.1	+0.8	346	<1.0	+0.2	7.4.10	3.1	+3.2
435	3.1	+3.0	839	<1.3	-0.8	345	<1.2	-0.5	7.4.11	0.8	+1.4
434	6.5	+4.9	8.3.10	<1.5	+1.0	344	3.2	+2.0	7.4.12	<0.4	-0.1
433	2.6*	+0.5	8.3.11	1.4	+1.8	343	5.8	+4.6	841	<1.3	+0.2
432	<1.8	-1.0	8.3.12	1.0	-1.0	342	2.7	+4.6	842	3.4	+4.3
431	1.1	+2.1	932	4.7	+5.6	341	2.2	-3.9	843	<0.7	-0.7
431	<1.4	-0.1	933	<1.2	-0.2	341	10.0	+11.7	844	<1.0	0.0
432	<1.3	+0.4	934	<1.4	+0.3	342	2.6*	+1.0	845	2.3	+0.9
433	<1.3	-1.3	935	5.8	+5.7	343	5.0	+10.0	846	4.7	-4.4
434	9.3	+9.7	936	<1.1	-1.0	344	15.1	+17.5	847	<1.2	-1.4
435	10.4	+9.7	937	1.5	-1.2	345	3.6	-4.9	848	<0.9	+1.3
436	3.5	+3.8	938	<1.1	+1.8	346	8.8	-10.2	849	<1.0	-1.0
437	<1.7	+1.4	939	<0.9	-1.2	347	<1.3	+2.0	8.4.10	3.1	-2.1
438	4.9	-6.6	9.3.10	<1.0	+0.2	348	3.7	-3.9	8.4.11	2.5	-3.0
439	2.7	-3.0	9.3.11	<1.1	+0.1	349	3.5	-4.0	944	<0.4	-0.9
4.3.10	3.6	+4.0	10.3.5	<0.6	+1.0	3.4.10	2.2	+2.2	945	<1.6	-1.2
4.3.11	<1.7	+0.9	10.3.6	<0.9	+0.1	3.4.11	<0.9	-0.3	946	<0.9	+2.0
4.3.12	<1.3	-1.1	10.3.7	<1.0	-0.6	446	<1.3	-1.0	947	3.4	+2.5
4.3.13	<0.6	-2.6	10.3.8	<1.0	+0.7	445	2.7	-1.4	948	<0.8	-0.5
535	<1.2	+0.7	10.3.9	<0.9	+0.5	444	3.1	-1.8	949	1.4	-1.8
534	2.2	+2.4	10.3.10	<0.6	-1.8	443	4.7	-4.5	9.4.10	<0.6	+2.0
533	<1.7	-2.0	041	4.5	-3.5	442	<1.7	-0.1	051	<1.8	-1.1
532	<1.6	+1.8	042	<1.6	+0.8	441	0.9	-0.6	052	<1.8	+1.0
531	<1.8	-0.2	043	1.4	-0.7	441	6.1	-4.6	053	11.3	-9.4

Table 3. (cont.)

<i>hkl</i>	<i>F</i> _{meas.}	<i>F</i> _{calc.}	<i>hkl</i>	<i>F</i> _{meas.}	<i>F</i> _{calc.}	<i>hkl</i>	<i>F</i> _{meas.}	<i>F</i> _{calc.}	<i>hkl</i>	<i>F</i> _{meas.}	<i>F</i> _{calc.}
054	5.4	- 5.8	3.5.10	1.2	- 1.8	064	3.3	+ 2.5	561	< 0.9	0.0
055	2.6	+ 3.2	455	< 1.2	- 3.7	065	4.3	- 4.3	562	< 1.1	+ 2.0
056	< 1.7	- 0.5	454	< 1.6	- 1.3	066	4.0	- 1.8	563	3.2	- 3.5
057	2.6	+ 1.8	453	2.2	+ 3.0	067	< 0.9	- 0.7	564	3.4	- 2.2
058	3.8	+ 4.0	452	< 1.5	+ 1.6	160	< 1.5	- 1.2	565	1.6	- 0.3
059	< 0.8	- 1.5	451	4.6	- 3.8	260	2.0*	+ 0.1	566	4.4	- 4.6
150	< 1.7	+ 2.9	451	3.7	+ 4.4	360	1.2	- 2.0	567	5.5	- 3.3
250	2.1	- 2.2	452	3.8	+ 2.5	460	1.0	- 0.5	568	2.4	- 1.4
350	2.0	- 1.3	453	2.8*	+ 0.3	560	< 0.6	- 0.1	569	< 0.4	- 1.0
450	4.1	- 4.3	454	7.5	+ 7.9	166	4.1	- 3.7	661	< 1.2	- 0.6
550	3.6	- 2.0	455	3.9	- 2.8	165	3.1	- 1.7	662	1.9	- 1.4
650	< 2.3	- 2.3	456	10.3	- 10.8	164	3.0	- 1.3	663	3.2	- 1.6
750	< 0.8	+ 0.5	457	< 1.5	+ 0.1	163	8.6	- 6.9	664	5.1	- 3.6
158	< 0.8	- 2.0	458	< 1.1	+ 0.8	162	6.6	- 4.5	665	< 1.0	- 1.5
157	3.1	- 2.6	459	0.7	- 1.3	161	3.5	- 2.6	666	3.8	+ 5.6
156	3.1	- 1.0	4.5.10	< 1.6	+ 1.4	161	1.2	+ 2.3	667	2.8	+ 3.5
155	< 1.7	- 0.9	4.5.11	< 1.0	+ 0.3	162	3.2	+ 1.6	668	3.1	- 3.8
154	2.6*	+ 0.6	553	< 1.3	- 2.0	163	5.9	+ 4.6	764	< 0.5	- 3.4
153	7.9	+ 7.4	552	1.7	- 1.9	164	2.8	+ 3.0	765	< 0.9	- 0.1
152	1.5*	+ 1.0	551	2.1	- 1.7	165	< 1.1	- 0.4	071	3.5	- 2.4
151	3.3	- 5.1	551	3.9	- 2.2	166	3.8	+ 3.2	072	1.6	- 0.9
151	1.2	- 2.4	552	4.0	- 4.0	167	< 1.2	+ 1.1	073	< 1.3	- 1.2
152	< 1.5	- 0.7	553	< 1.9	- 0.3	168	< 0.8	- 1.6	074	< 1.1	+ 0.8
153	11.3	+ 11.8	554	< 1.5	+ 2.0	265	3.2	- 3.0	075	1.4	- 0.6
154	8.2	+ 5.9	555	1.7	+ 1.0	264	< 1.2	+ 0.3	170	1.9	+ 0.9
155	4.5	+ 2.3	556	7.1	+ 6.5	263	7.5	+ 7.4	270	< 1.2	- 1.0
156	3.5	+ 4.1	557	4.7	+ 4.2	262	3.0	+ 2.3	370	< 0.8	+ 0.1
157	2.3	- 1.6	558	1.8	- 2.8	261	4.8	- 5.7	470	< 0.8	+ 0.9
158	2.8	- 2.4	559	< 1.0	+ 0.8	261	< 1.5	+ 0.4	174	< 0.8	+ 0.1
159	< 1.1	- 1.0	5.5.10	5.8*	+ 0.1	262	1.7	- 2.7	173	2.3	+ 2.6
257	< 0.8	+ 3.1	652	< 1.7	+ 1.9	263	2.6	+ 3.5	172	< 1.0	+ 0.4
256	1.6	- 1.6	651	< 1.6	- 0.9	264	2.0	+ 1.6	171	1.5	- 1.8
255	4.7	- 3.5	651	< 0.8	+ 1.8	265	< 1.5	- 2.0	171	1.8	- 1.4
254	2.8	- 1.1	652	4.9	+ 5.2	266	< 1.1	+ 0.5	172	4.4	- 4.4
253	2.3	- 1.6	653	< 1.3	- 0.9	267	1.6	- 0.4	173	2.5	- 1.2
252	2.3*	- 0.3	654	2.6	- 1.4	268	< 0.9	- 0.2	174	< 1.0	+ 0.3
251	2.9	- 3.7	655	< 1.4	- 0.2	364	< 0.7	+ 0.2	175	1.6	- 1.4
251	< 1.6	+ 2.7	656	3.9	- 4.7	363	3.8	- 3.9	273	3.2	- 4.5
252	< 1.6	- 2.3	657	2.8	- 1.6	362	4.4	- 3.9	272	4.1	- 1.7
253	9.1	+ 7.9	658	< 1.6	+ 0.3	361	1.8	- 0.8	271	< 1.5	+ 1.7
254	10.1	+ 12.5	659	1.0	- 1.7	361	< 1.2	+ 1.2	271	1.5**	+ 2.1
255	6.5	- 7.1	6.5.10	< 0.7	+ 0.3	362	< 1.3	+ 0.3	272	< 1.2	+ 1.8
256	7.0	- 7.0	6.5.11	< 0.3	- 0.5	363	< 1.5	+ 1.7	273	2.1	- 2.7
257	< 1.5	+ 1.4	751	< 1.4	- 1.6	364	< 1.2	+ 1.5	274	1.9	- 2.2
258	2.7	- 2.7	752	2.7	- 2.2	365	2.0	- 1.2	275	1.2	+ 1.2
259	< 1.1	- 0.1	753	2.9	- 2.3	366	1.4	- 1.8	276	2.9	+ 3.5
2.5.10	3.5	+ 3.1	754	3.1	- 1.7	367	< 0.9	+ 0.5	371	< 1.3	+ 1.7
356	< 0.6	- 2.1	755	2.2	- 1.5	368	1.4	- 1.3	371	< 0.9	+ 0.2
355	3.3	- 2.5	756	1.6	+ 1.5	369	< 0.5	+ 0.2	372	3.0	- 3.1
354	1.6	- 1.9	757	2.1	+ 2.5	463	< 0.9	+ 1.7	373	3.6	- 3.7
353	< 1.3	+ 0.5	758	1.4	- 2.4	462	2.6	+ 2.0	374	1.8	- 1.1
352	1.2	- 2.5	759	2.2	- 1.0	461	< 0.8	- 0.8	375	< 0.8	- 0.4
351	4.3	- 4.9	7.5.10	< 0.7	+ 0.8	461	< 1.3	+ 1.0	376	2.7	- 1.8
351	3.2	- 1.4	853	< 0.4	+ 0.9	462	< 1.8	- 1.0	471	< 0.7	- 0.6
352	2.1	- 3.5	855	2.3	- 1.8	463	2.6	- 1.2	472	1.6	+ 1.9
353	5.8	+ 6.9	856	< 1.1	+ 1.0	464	3.0	- 2.5	473	2.2	- 2.9
354	7.1	+ 6.6	857	< 0.8	+ 0.3	465	< 1.4	- 0.5	474	1.5	- 2.7
355	4.4	+ 3.6	858	1.8	- 1.3	466	5.3	+ 5.1	475	< 1.3	+ 1.1
356	7.4	+ 8.7	859	< 0.6	- 2.6	467	< 1.1	+ 0.9	476	< 1.5	+ 1.3
357	2.3	+ 2.2	061	4.2	- 4.6	468	3.0	- 2.4			
358	2.0	- 2.5	062	< 1.8	- 1.6	469	< 1.9	+ 0.7			
359	< 1.0	+ 0.7	063	8.8	+ 8.9	561	< 1.3	+ 2.0			